

(12) UK Patent Application (19) GB (11) 2 279 095 (13) A

(43) Date of A Publication 21.12.1994

(21) Application No 9411505.2

(22) Date of Filing 09.06.1994

(30) Priority Data

(31) 08078123 (32) 15.06.1993 (33) US

(71) Applicant(s)

Smith International Incorporated

(Incorporated in USA - Delaware)

PO Box 60068, 16740 Hardy Street, Houston,
Texas 77205-0068, United States of America

(51) INT CL⁵

E21B 10/52 10/16

(52) UK CL (Edition M)

E1F FFD

(56) Documents Cited

GB 2274129 A EP 0476352 A1 US 5119714 A

US 4940099 A

(58) Field of Search

UK CL (Edition M) E1F FFD FGA FGB FGC

INT CL⁵ E21B 10/52

Online databases: WPI

(72) Inventor(s)

Michael A Siracki

Chris E Cawthorne

Scott D McDonough

Gary Portwood

(74) Agent and/or Address for Service

Saunders & Dolleymore

9 Rickmansworth Road, WATFORD, Herts, WD1 7HE,
United Kingdom

(54) Ultra hard insert cutters for heel row rotary cone rock bit applications

(57) A rotary cone rock bit for drilling boreholes in an earthen formation is disclosed. One or more rotary cones 16 are rotatably retained on a journal bearing 19 connected to the rock bit. These rotary cones 16 form a circumferential heel row 30 with extended ultra hard shaped cutters 38 spaced within the heel row. Each of the shaped cutters 38 form a cutting surface that extends above the heel row or is angled with respect to the formation to maintain the cutters in compression while the cutters shear a borehole wall. The shaped cutters serve to maintain the borehole diameter.

FIG. 2

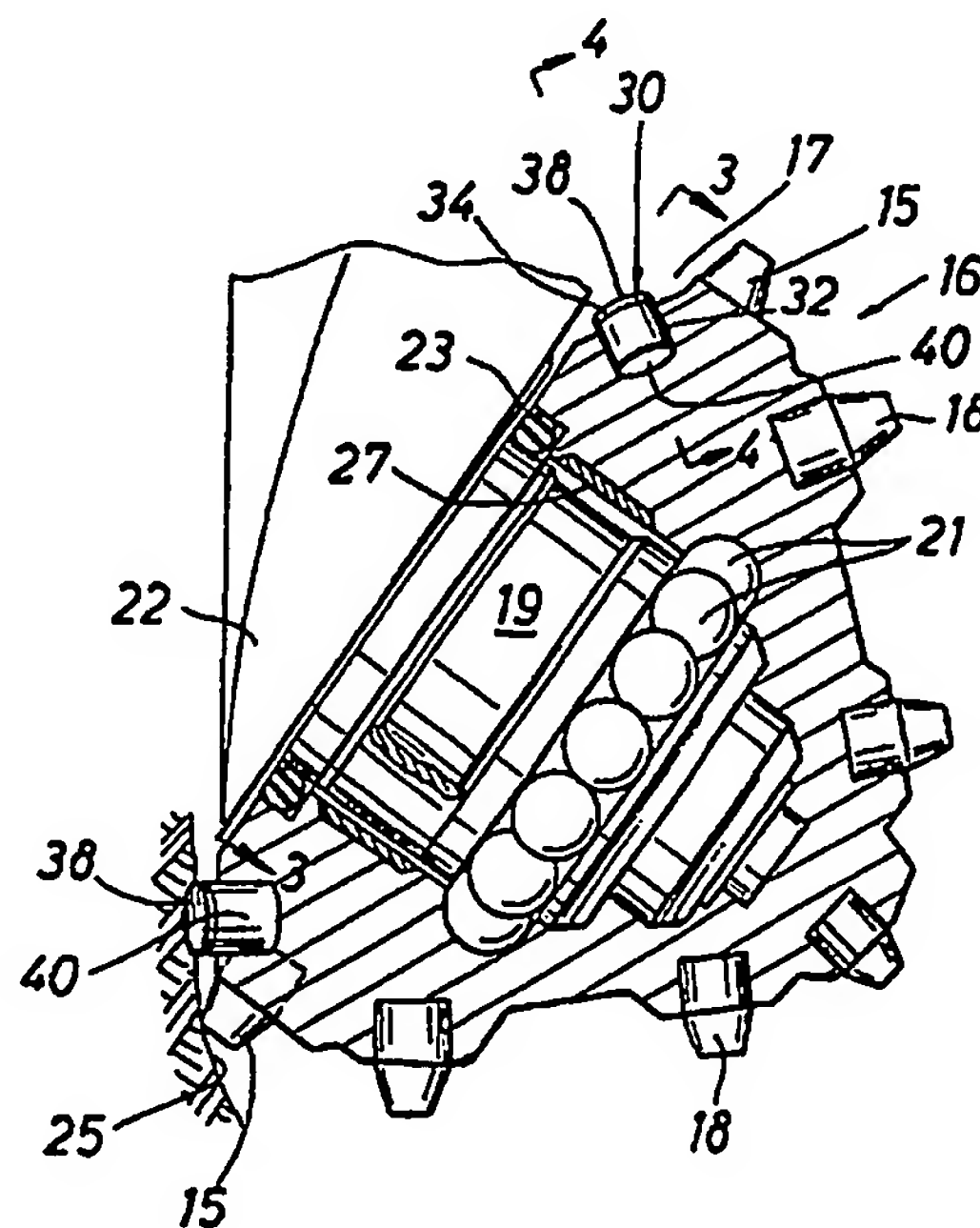


FIG. 1

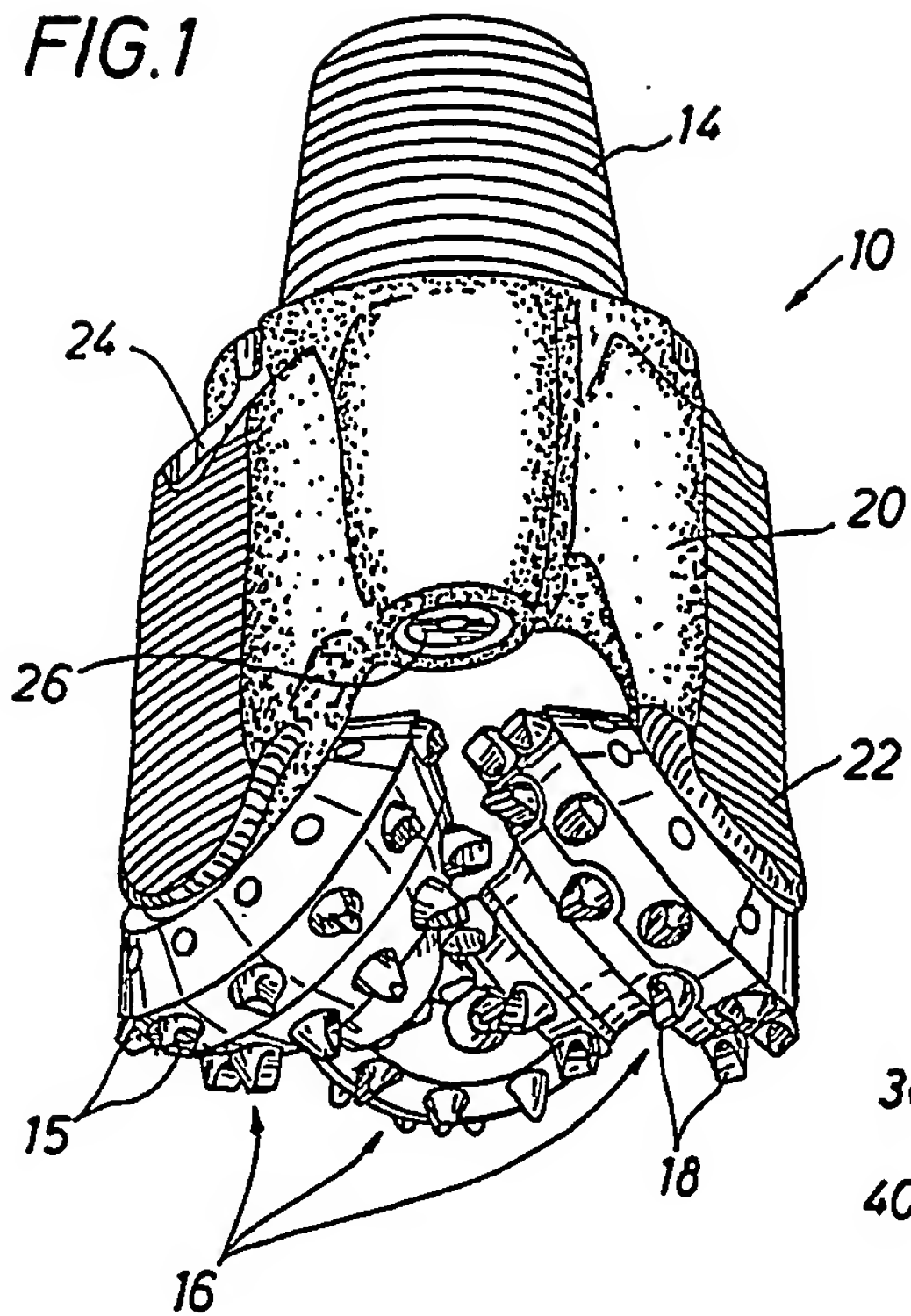


FIG. 2

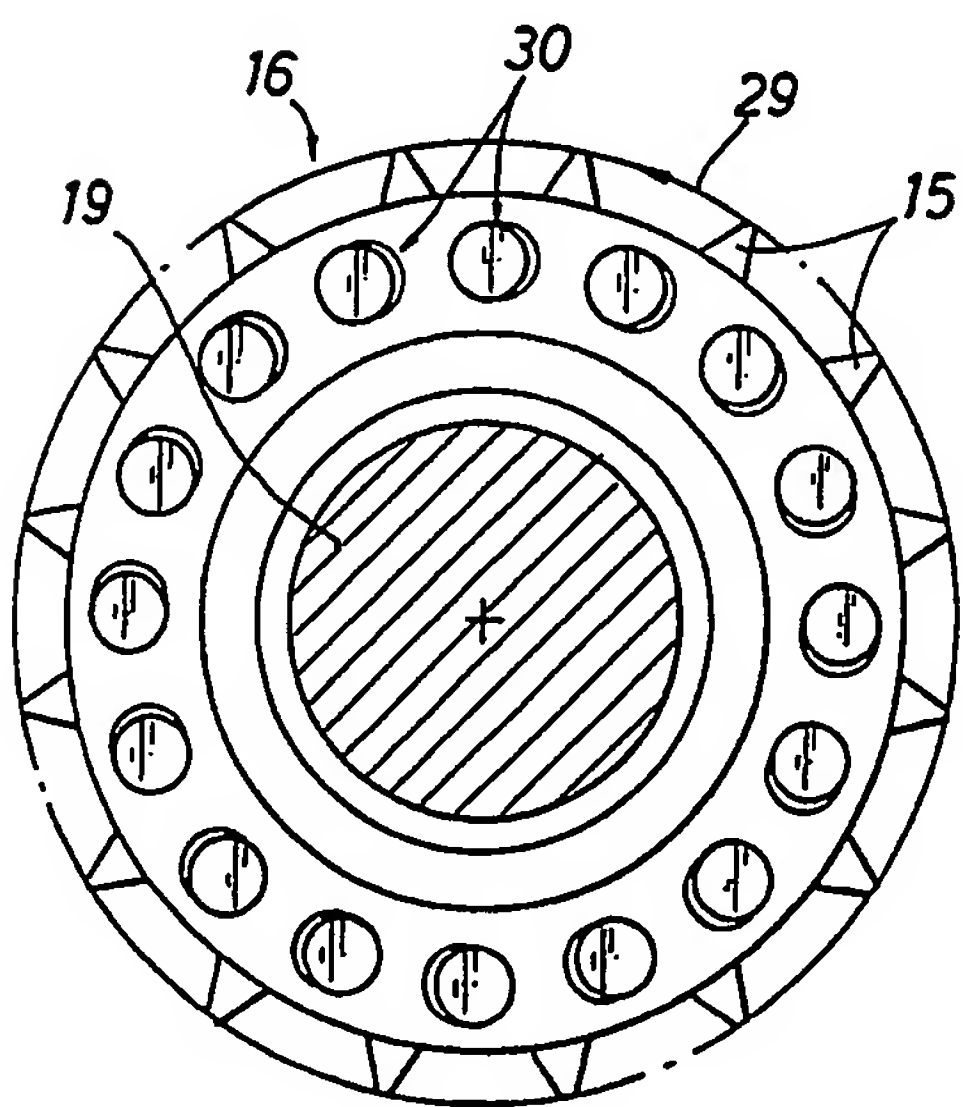
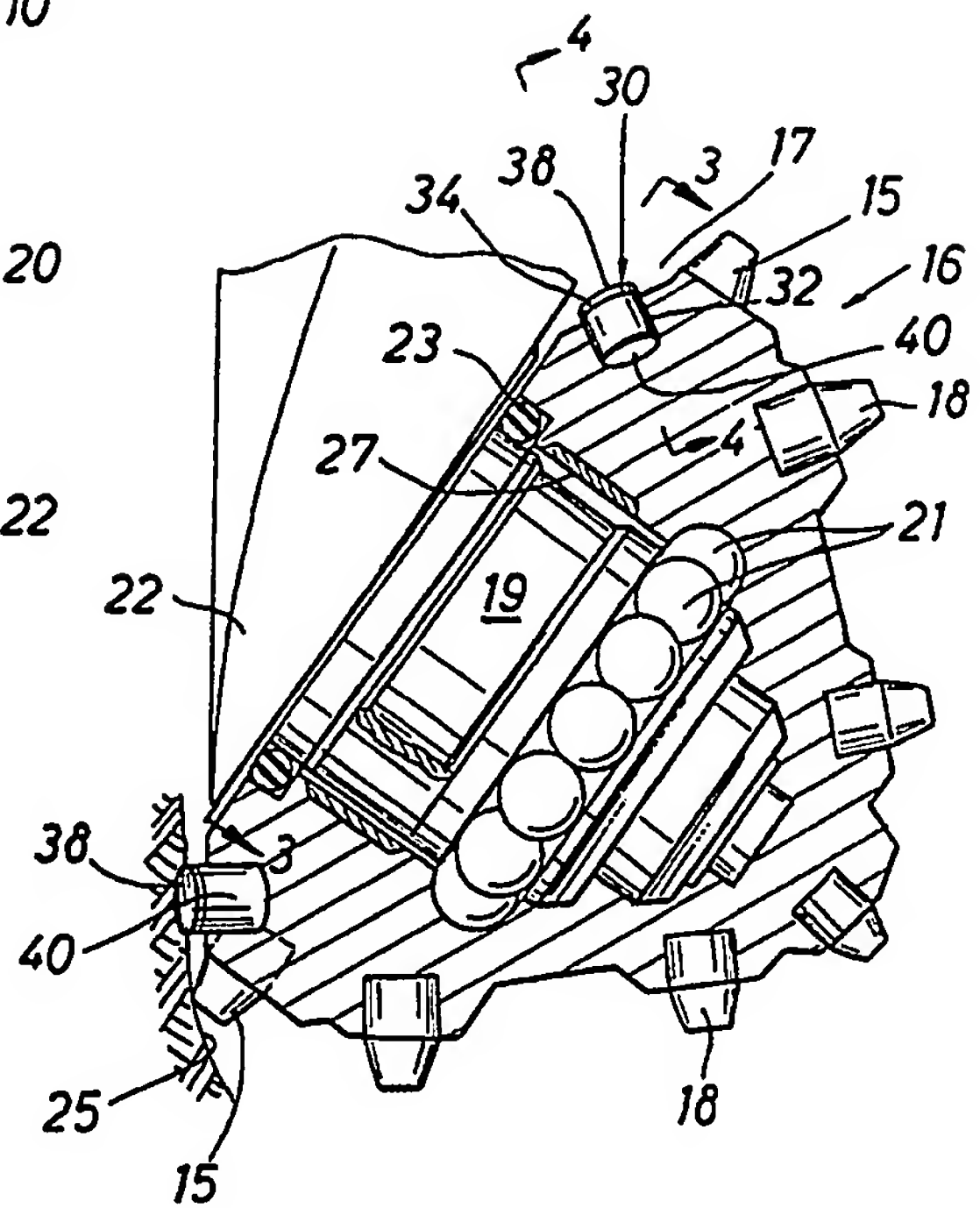


FIG. 3

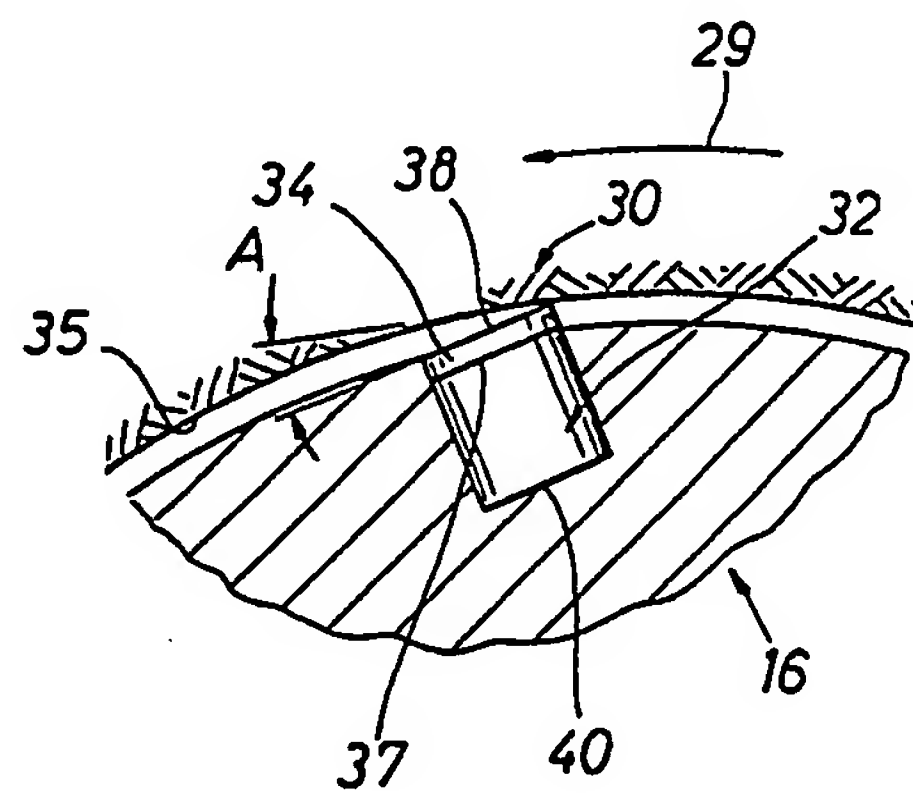
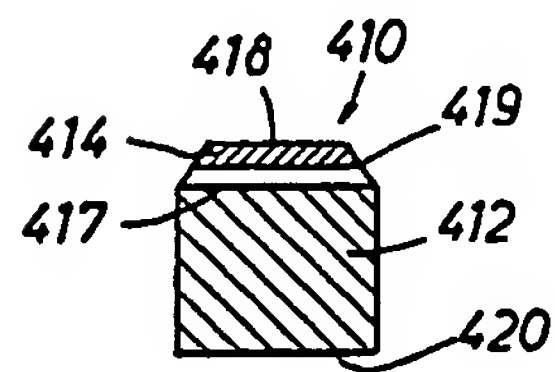
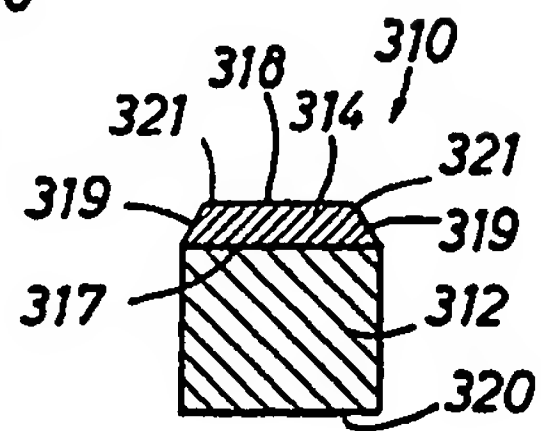
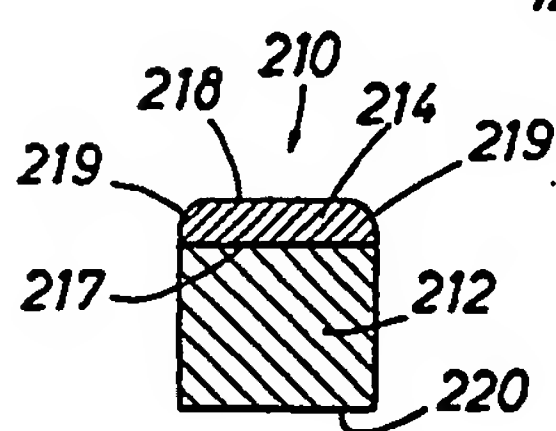
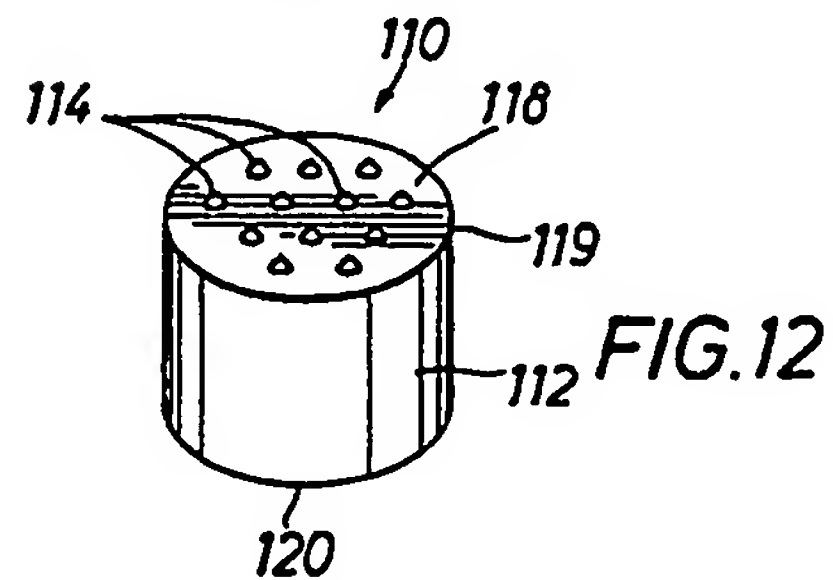
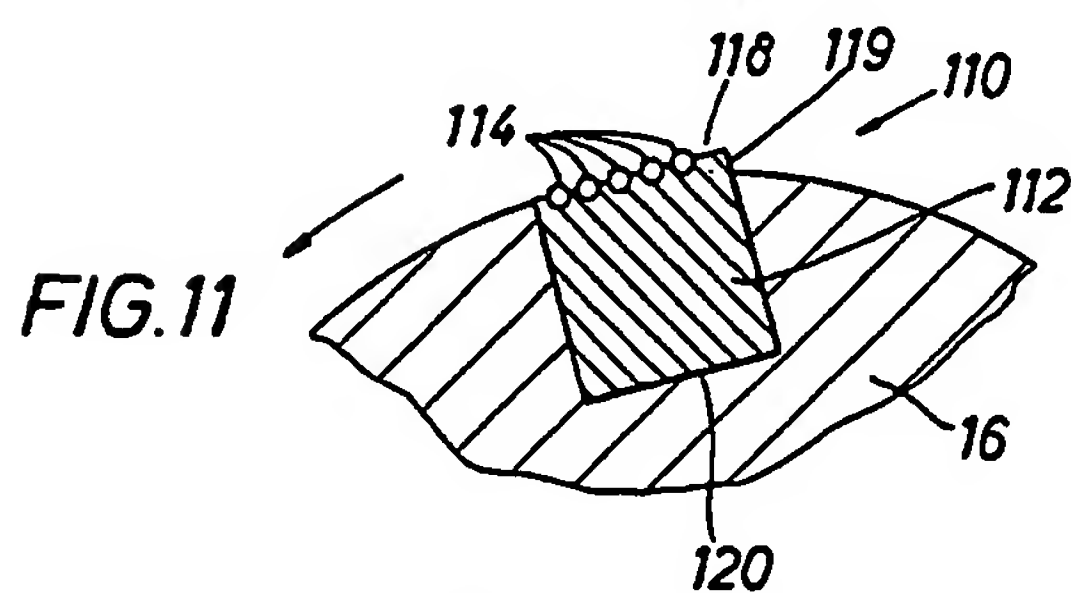
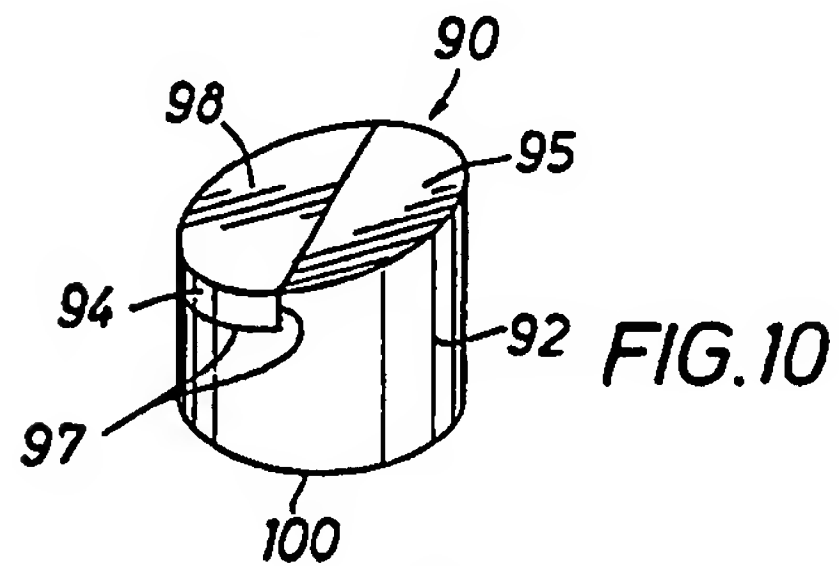
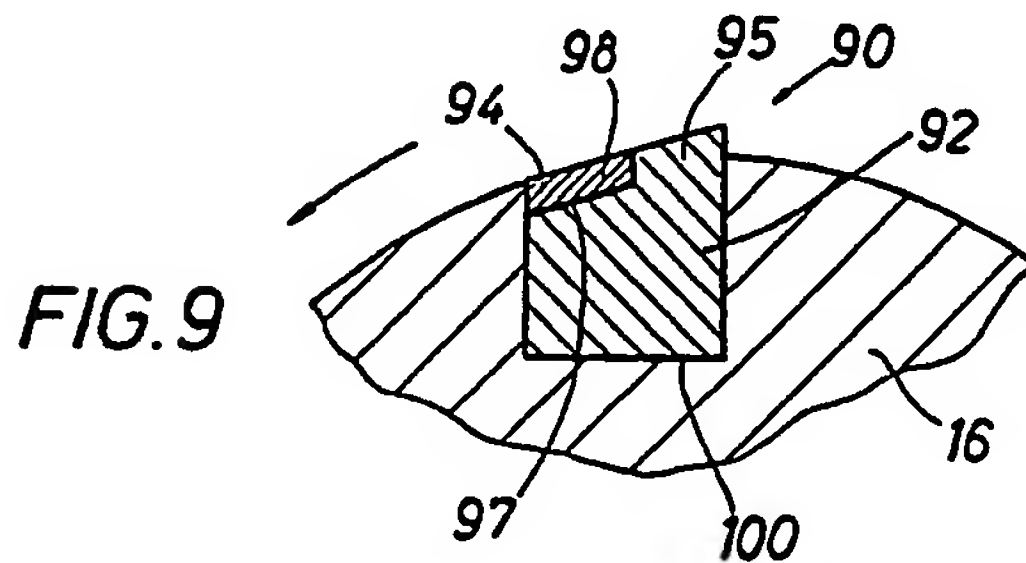
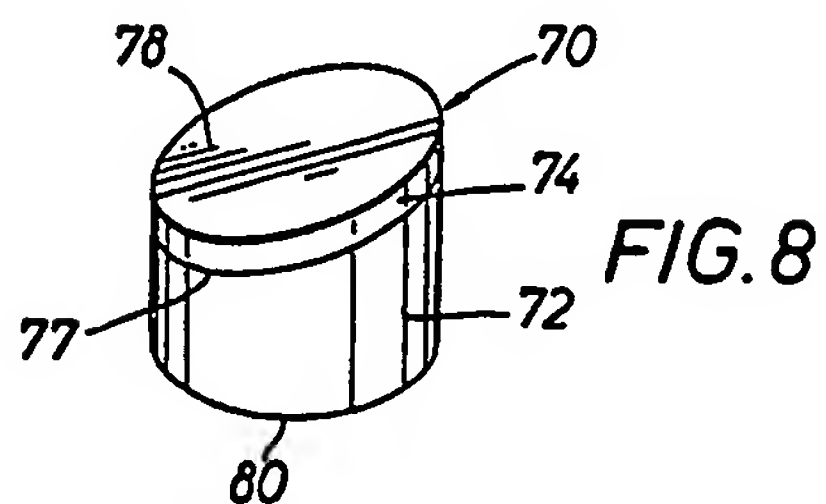
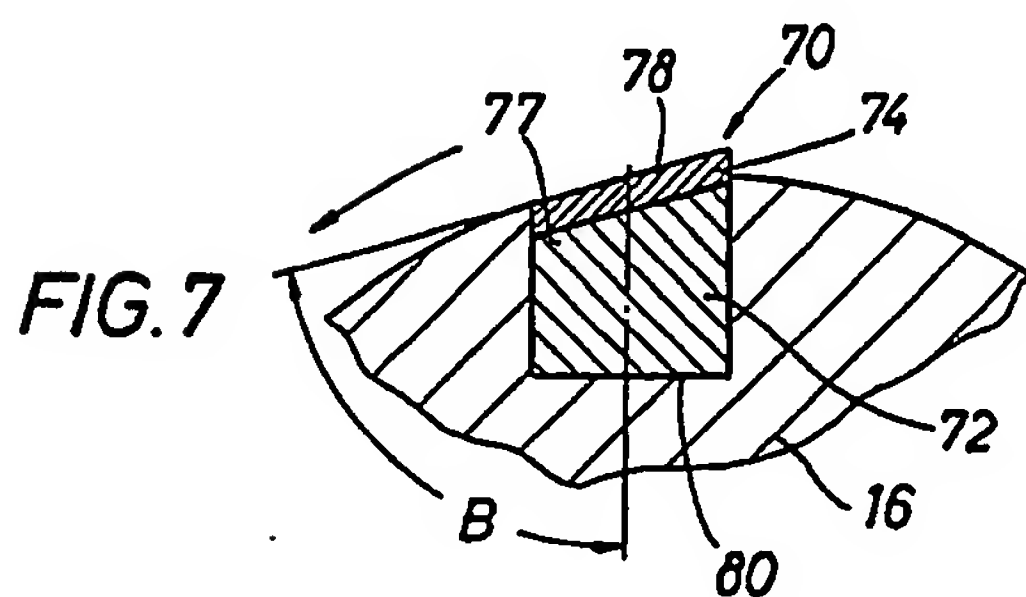
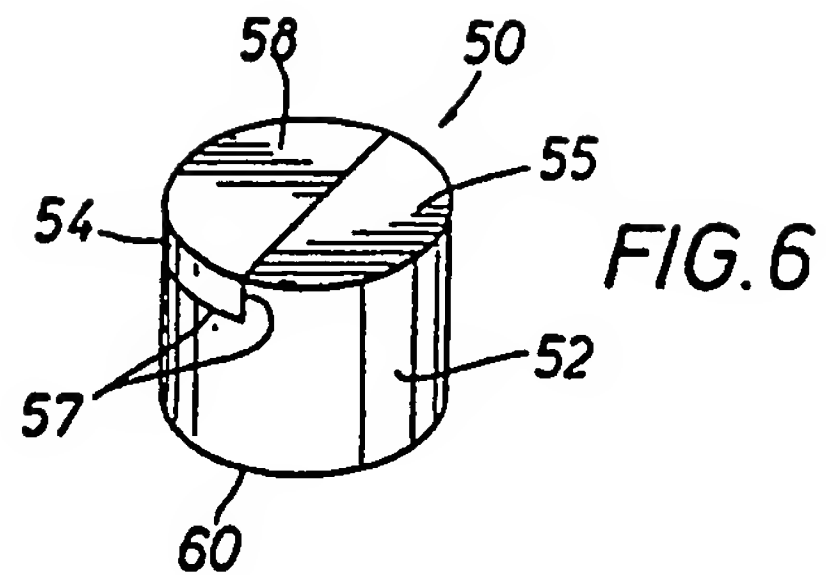
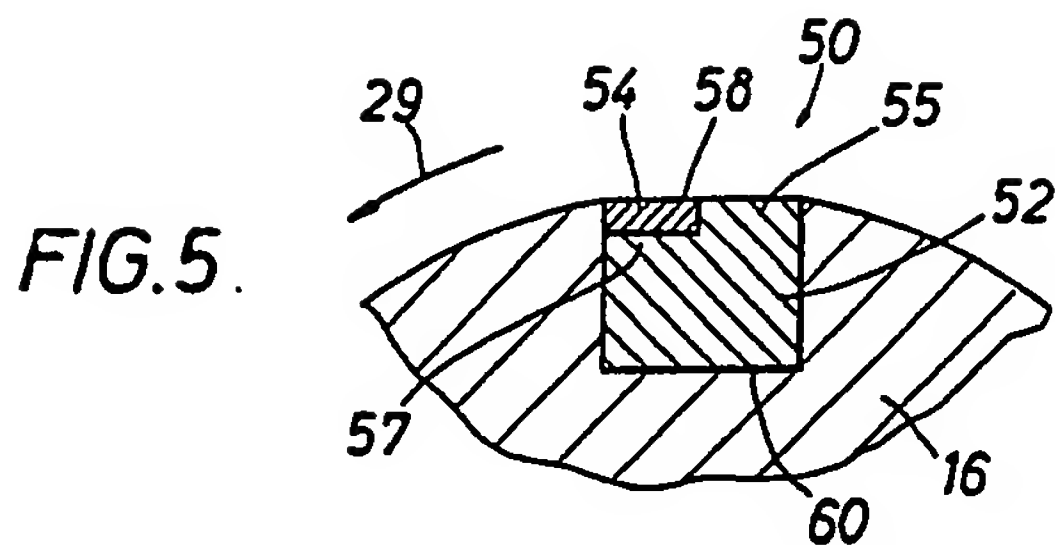


FIG. 4



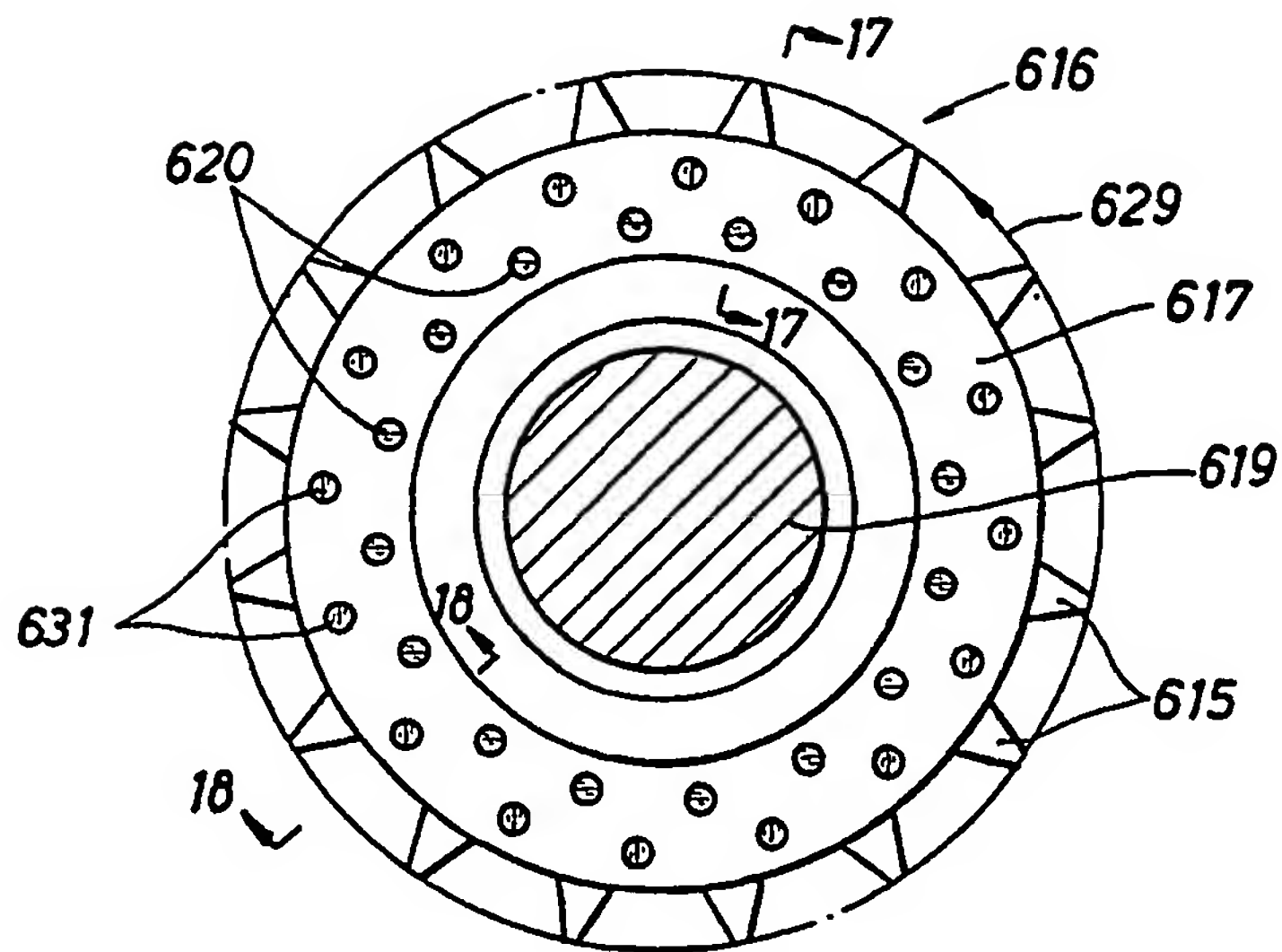


FIG. 16

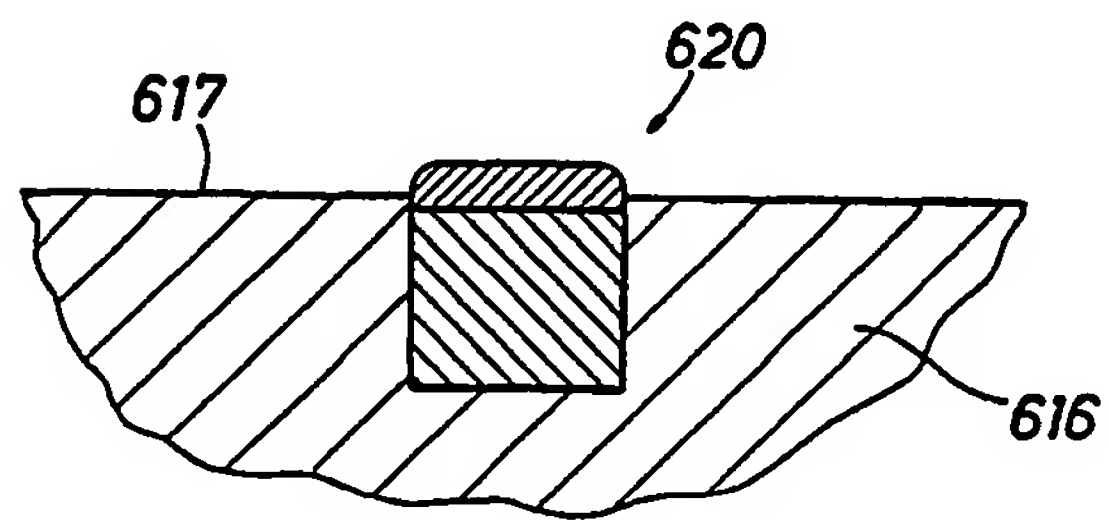
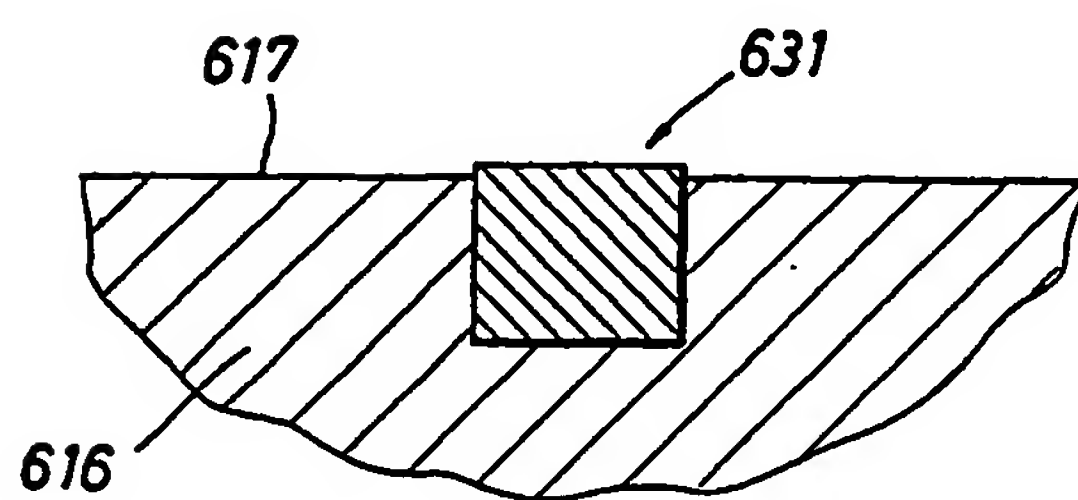


FIG. 18

FIG. 17



1

5

10

ULTRA HARD INSERT CUTTERS FOR HEEL ROW
ROTARY CONE ROCK BIT APPLICATIONS

15

This invention relates to the cutting structure formed on rotary cones of rotary cone rock bits utilized to drill boreholes in an earthen formation.

20

More particularly, this invention relates to the use of shaped diamond or other ultra hard material insert cutters in the heel row of each of the rotary cones associated with the drill bit for maintaining the gage bore diameter of the formation. These ultra hard materials include cubic boron nitride and/or diamond/refractory metal carbide composites.

25

Diamond inserts in roller cone rock bits have been tried before in an attempt to extend the useful life of a rock bit as it works in a borehole.

30

U.S. Patent Number 4,940,099 teaches the utilization of alternating tungsten carbide inserts and diamond inserts in each row formed on a rock bit cutter cone. Both the heel row and the gage row as well as successive concentric rows terminating at the apex of the truncated cone alternate tungsten carbide chisel inserts with diamond inserts. The heel row adjacent the cone mouth opening alternates flush mounted tungsten carbide inserts with harder tungsten carbide flush inserts with a layer of diamond bonded thereto. The alternating gage row inserts extend from the cone surface and serve to cut the gage of the borehole which of course determines the diameter of the drilled hole in the earthen formation.

35

It is well known in the art to utilize flush type inserts in the heel row of roller cones primarily to minimize erosion of the cones due to the passage of drilling fluid and formation detritus between the heel and gage rows of the cones and the borehole wall. The '099 patent, while it teaches alternating hard and soft flush inserts in the heel row also teaches that it is more important that the

1 larger diameter rows, particularly the gage row, be provided with an intermingled
pattern of soft and hard inserts to facilitate drilling differing earthen formations.

Maintenance of a constant diameter borehole throughout the drilling
operation is of paramount importance in controlling cost-per-foot drilling costs.
5 If a rock bit should drill undergage it results in a following, same diameter bit to
pinch due to the undersized hole condition. This usually results in a ruined rock
bit and is the cause of another trip out of the hole followed by a reaming
operation, all of which is time consuming and very costly.

Flush type heel row inserts ultimately act as a passive bearing surface
10 when the heel of the cone is in contact with the borehole wall. When the entire
heel surface of each of the cones is in contact with the borehole wall, the cones
are subjected to tremendous in-thrust loads. The in-thrust loads tend to pinch
the bit, damage the cone and journal bearings and cause heat checking of the
tungsten carbide inserts.

15 U.S. Patent Number 5,131,480, hereby incorporated by reference,
teaches the use of extended tungsten carbide inserts in a recessed heel row in
a milled tooth rotary cone rock bit. While this patented feature greatly improved
directional drilling capabilities, the rounded projections on the heel row inserts
somewhat limited the rock shearing function necessary for aggressive side
20 cutting while turning from a straight drill run.

It was found through experimentation that if drilling energy is not put into
shearing the rock, the energy then converts into pushing the cone away from the
rock formation resulting in the heretofore mentioned in-thrust condition with all
of its disadvantages.

25

A rotary cone rock bit for drilling boreholes in an earthen formation has
one or more rotary cones rotatively retained on a journal bearing connected to
a body of the rock bit. Each cone comprises a circumferential heel row with
30 extended ultra hard cutters spaced within the heel row. Each of the shaped
cutters comprises a surface that protrudes into the earthen formation as the
rotary cone rotates against a bottom of the borehole formed by the formation.
The shaped cutters serve to maintain the borehole diameter.

Preferably, each of the inserts comprises a diamond cutting surface that
35 is angled with respect to the formation to maintain the inserts in compression
while the diamond inserts maintain a substantially constant borehole diameter as
the rotary cone rotates against a bottom of the borehole.

1 In one embodiment, such a diamond insert is a right angle cylindrical body
with an edge formed by the cylinder at the exposed diamond surface chamfered
or radiused to reduce cracking and chipping of the diamond.

5 If desired, two or more rows of heel inserts are positioned different radial
distances from a cone axis, at least one row containing diamond faced inserts,
the diamond faced inserts being on a shorter radial distance than another heel
row containing inserts formed from tougher ultra hard material such as cemented
tungsten carbide.

10 The inserts serve to maintain a constant diameter borehole wall formed
by the formation as the rotary cone rotates against a bottom of the borehole.

15 The above noted features and advantages of the present invention will be
more fully understood upon a study of the following description in conjunction
with the detailed drawings wherein:

FIGURE 1 is a perspective view of a sealed bearing rotary cone rock bit;

FIGURE 2 is a partially cut away cross-section of a roller cone mounted
to a journal bearing;

20 FIGURE 3 is an end view of the cone taken through 3-3 of Figure 2
illustrating the heel surface of the cone and the orientation of each of the
diamond cutters equidistantly placed around the heel row;

25 FIGURE 4 is a view taken through 4-4 of Figure 3 illustrating the
orientation of one of the heel row inserts with the forward edge of the insert
about even with the surface of the cone and the trailing edge of the insert
protruding from the cone surface;

30 FIGURE 5 is an alternative heel row insert for the insert depicted in Figure
4, the insert being mounted substantially even with the surface of the cone,
about one half of the circular cutting end of the insert is diamond and the other
half is tungsten carbide, the diamond half being oriented toward the direction of
rotation of the cone;

FIGURE 6 is a perspective view of the insert shown in Figure 5;

35 FIGURE 7 is another alternative heel row insert for the insert depicted in
Figure 4 the top or cutting end of the cylindrical insert is cut at an oblique angle
such that when the insert is positioned within a retention hole drilled in the cone
substantially ninety degrees to the cone surface, a trailing edge portion of the
diamond capped end of the insert extends beyond the surface of the cone when

1 a leading edge of the insert is positioned toward the direction of rotation of the cone;

FIGURE 8 is a perspective view of the insert shown in Figure 7;

5 FIGURE 9 is a variation of the insert illustrated in Figures 7 and 8 wherein the leading edge half of the slanted top of the insert is diamond and the raised trailing edge is cemented tungsten carbide;

FIGURE 10 is a perspective view of the insert shown in Figure 9;

10 FIGURE 11 is yet another alternative heel row insert that may be used in place of the insert shown in Figure 4 wherein the cutting surface of the insert comprises a layer of diamond particles imbedded in a matrix of a tungsten carbide;

FIGURE 12 is a perspective view of the insert shown in Figure 11;

FIGURE 13 is a diamond capped cylindrical heel row insert with the diamond cutting edge rounded;

15 FIGURE 14 is a diamond capped cylindrical heel row insert with the diamond cutting edge chamfered, the cutting edge at the end of the chamfered diamond being slightly rounded;

20 FIGURE 15 is a diamond capped cylindrical heel row insert, the chamfered diamond cutting end being smaller in diameter than the diameter of the cylindrical body;

25 FIGURE 16 is an end view of a roller cone with emphasis on the heel row of the cone illustrating staggered rows of flush type tungsten carbide near the outer diameter of the heel row with diamond heel row inserts strategically placed in the heel row between the bearing cavity formed by the cone and the outer row of tungsten carbide inserts;

FIGURE 17 is a view taken through 17-17 of Figure 16 illustrating a standard tungsten carbide flush type insert mounted in a heel surface of the cone; and

30 FIGURE 18 is a view taken through 18-18 of Figure 16 illustrating a slightly raised diamond capped insert with a rounded edge such as shown in Figure 13.

35 Boreholes are commonly drilled with rock bits having rotary cones with cemented carbide inserts interference fitted within sockets formed by the cones. Such a rock bit generally designated as 10 has a steel body 20 with threads 14 formed at an upper end and three depending legs 22 at its lower end. Three

1 cutter cones generally designated as 16 are rotatably mounted on three legs 22
at the lower end of the bit body. A plurality of cemented tungsten carbide
inserts 18 are press-fitted or interference fitted into insert sockets formed in the
surface of the cones 16. Lubricant is provided to the journals 19 (Fig. 2) on
5 which the cones are mounted from each of three grease reservoirs 24 in the
body 20.

When the rock bit is used, it is threaded onto the lower end of a drill
string and lowered into a well or borehole. The bit is rotated with the carbide
inserts in the cones engaging the bottom of the hole. As the bit rotates, the
10 cones 16 rotate on the bearing journals 19 or roller bearings (not shown)
cantilevered from the body and essentially roll around the bottom of the borehole
25 (Fig. 2). The weight of the bit is applied to the rock formation by the carbide
inserts 18 and the rock is thereby crushed and chipped by the inserts. A drilling
fluid is pumped down the drill string to the bottom of the hole and ejected from
15 the bit body through nozzles 26. The drilling fluid then travels up the annulus
formed between the outside drill pipe wall and the borehole formation walls. The
drilling fluid provides cooling and removes the chips from the bottom of the
borehole.

With reference now to Figure 2, the lower portion of the leg 22 supports
20 a journal bearing 19 on which the cone 16 rotates. The cone is retained on the
bearing 19 by a plurality of cone retention balls 21 confined by a pair of opposing
ball races formed in the journal and the cone. The cone comprises an annular
heel row 17 positioned between the gage row inserts 15 and a bearing cavity 27
formed in the cone 16. A multiplicity of protruding heel row insert cutters
25 generally designated as 30 are about equidistantly spaced around the heel row
17. The protruding inserts 30 and the gage row inserts 15 coact to primarily cut
the gage diameter of the borehole 25. The multiplicity of remaining inserts 18
in concentric rows crush and chip the earthen formation as heretofore described.

With reference now to Figures 3 and 4, each of the heel row cutters 30
30 is, for example, formed from a cemented tungsten carbide body 32 having a base
end 40 and a cutter end 38. The cutter end supports an ultra hard cutter
element 34 (preferably polycrystalline diamond) that is, for example,
metallurgically bonded or brazed to the cutting end at juncture 37.

Each of the diamond inserts 30 is preferably interference fitted within
35 insert retention sockets 31 formed in heel row 17 (Fig. 4).

The diamond material may be composed of polycrystalline material
pressed in a super pressure press of the type taught in U.S. Patent Number

1 4,604,106. Moreover, the diamond cutters may be fabricated from a composite
of tungsten carbide material impregnated with diamond particles. The process
is set forth in U.S. Patent Numbers 4,966,627 and 5,045,092.

5 Additionally, the previously described ultra hard inserts may be fabricated
from composites of cubic boron nitride (CBN) and refractory metal carbides such
as tungsten carbide.

10 Insert 30 comprises a full diamond disc, the leading edge 33 of which is
about flush or even with the heel surface 17 of cone 16. The trailing edge 35
extends above the heel surface 17 and is exposed to the earthen formation 25.
Thus, the diamond cutting surface is angled with respect to the formation. That
is, the cutting surface is angled relative to a tangent to the heel surface 17 of the
cone. As the cone 16 is rotated in direction 29 by the drill string, the diamond
surface 38 is subjected to compressive forces by the formation 25. This
angulation of the diamond cutting face 38 (5 to 25 degrees from the borehole
15 wall 35) maintains the PCD disc in compression to reduce shear failures due to
the thermal mismatch between the diamond disc 34 and the tungsten carbide
insert body 32. The preferred angulation is 5 degrees (angle "A" Figure 4).

20 Referring now to Figures 5 and 6, an alternative heel row insert generally
designated as 50 is retained within a socket 31 formed in the heel row 17 of the
cone 16. The insert 50 comprises half a diamond disc 54 secured within a
recess 56 formed in surface 58 of a cemented carbide body 52. The half
diamond disc 54 is preferably bonded to the body 52 at juncture 57 and 59. The
backup support 55 formed by the insert body 52 will allow the trailing edge 59
of the cutter 50 to be supported to prevent diamond cutter breakage due to
25 elastic rebound of the formation against the cutters that often occurs during
drilling operations.

30 Figures 7 and 8 illustrate still another alternative embodiment wherein the
socket 31 in the cone 16 is aligned radially from an axis of the cone and the
insert generally designated as 70 has an angled surface 78 with respect to an
axis of the insert body 72. The angled surface (angle "B" Figure 7) is from 70
to 85 degrees from the axis of the insert. The diamond disc 74 is oriented with
its leading edge 73 substantially even or flush with the heel surface 17 and the
trailing edge 75 extending above the surface 17 similar to the insert 30 shown
in Figures 2, 3 and 4. An insert so configured might be needed where cone
35 material to support the heel row inserts is at a premium. For example, the insert
30 in Figures 2, 3 and 4 requires that the socket 31 be drilled at an angle to a
radial line from an axis of the cone 16. In this example, each insert 30

1 necessarily takes up more room in the heel surface, thus less of the heel row
inserts may be utilized as a result. Hence the insert 70 with the desired cutter
disc angulation might be preferred since, because of the radial orientation of the
sockets 31, there would be more room for additional inserts in the heel row.

5 Figures 9 and 10 depict a variation of insert 70. An insert generally
designated as 90 consists of half a disc 94 that is similar in fabrication to insert
50 except that the cutter surface is angled with respect to a axis of the insert
body 92.

10 The heel row insert 110 depicted in Figures 11 and 12 comprises a
tungsten carbide body 112, the surface 118 of which supports a multiplicity of
natural or synthetic diamonds cutters 114. The diamond particles 114 may be
metallurgically or mechanically secured to the surface 118 by state of the art
methods. Alternatively, the diamond particles may retained within a matrix of
tungsten carbide. In this example, the natural or synthetic diamonds are
15 normally set within a depression formed in an insert mold followed by the
insertion of a matrix of tungsten carbide powder and a binder such as cobalt into
the mold. The insert is subsequently sintered in a furnace.

20 As earlier illustrated and described, the trailing edge 119 of the insert 110
extends beyond surface the heel surface 17 of the cone 16, an axis of the body
12 being angularly displaced from a radial line from an axis of the cone.

Figures 13, 14, 15 and 16 are variations on flush type diamond heel row
inserts.

25 The insert 210 of Figure 13 is crowned with a synthetic diamond cap 214
bonded to a cemented tungsten carbide body 212 at junction 217 or the layer
of diamond may be a transition layer of diamond and tungsten carbide as
heretofore described. In this example the corners 219 of the diamond cap 214
are essentially one quarter round. The rounded corners are less apt to chip when
in operation in a borehole.

30 The insert may be mounted within the heel row 17 of cone 16 either
radially aligned (see Fig. 5) or aligned at an angle to a radial line with respect to
an axis of the cone as is shown in Figures 2 thru 4.

35 Figure 14 is another insert 310 with the diamond rim 319 chamfered.
The cutting edge 321 however is rounded again to minimize chipping of the
diamond at the corner 321 transitioning between the chamfered rim 319 and the
flat top surface 318.

The insert 410 shown in Figure 15 is also chamfered except that the
diamond cap 414 does not cover the entire cutting end of the insert. In other

1 words, the diamond is kept off of the outside diameter of the insert. This would
be of no consequence where the insert is inserted in an insert socket formed in
a cone such that the inside corner of the chamfer at the cutting end 418 of the
insert is below the heel row surface 17 of cone 16.

5 Figure 17 is a view of the back or heel surface 617 of a cone 616. This
view is similar to the previously described in Figure 3 except that there two rows
of inserts in heel surface 617. The row of inserts 620 nearest the journal
bearing 619 (shortest radial distance from an axis of the cone) are diamond
inserts of the type described in Figure 13. The outer row of inserts 631 in the
10 heel surface 617 and nearest the gage row inserts 615 preferably comprise an
insert fabricated from ultra hard material that is tougher than the row of diamond
inserts. Cemented tungsten carbide inserts of various grades of hardness are
examples of such inserts 631.

15 The purpose of the double row of inserts in heel surface 617 is to utilize
the tougher inserts 631 to bring the borehole to full or near full gage prior to the
engagement of the diamond inserts 620 to put less work on the diamonds, thus
preserving the life of the diamonds resulting in a more prolonged maintenance of
the borehole diameter during drilling operations. This is possible since tungsten
carbide is tougher than diamond.

20 Figure 17 depicts the insert 631 which may be positioned slightly above
the heel surface 617 as is shown in the drawing.

Figure 18 illustrates the diamond cutter 620 with rounded corners as
depicted in Figure 13. It should be noted that the diamond cap of the insert is
protected at the juncture to the carbide insert body by inserting the insert deeper
25 into its retention socket formed in the cone 616.

It will of course be realized that various modifications can be made in the
design and operation of the present invention without departing from the spirit
thereof. For example, one may use any of the insert cutter designs shown in
Figures 13 through 15 in place of the insert 30 shown in Figures 1 through 4.
30 Thus, while the principal preferred construction and mode of operation of the
invention have been explained in what is now considered to represent its best
embodiments, which have been illustrated and described, it should be understood
that within the scope of the appended claims, the invention may be practiced
otherwise than as specifically illustrated and described.

35

1 **CLAIMS**

1 1. A rotary cone rock bit for drilling boreholes in an earthen formation
comprising one or more rotary cones rotatably retained on a bearing connected
to a body of the rock bit, each cone comprising a circumferential heel row, with
5 extended inserts spaced within the heel row, and characterized by

 each of the inserts comprising a diamond cutting surface that is angled
with respect to the formation to maintain the inserts in compression while the
diamond inserts maintain a substantially constant borehole diameter as the rotary
cone rotates against a bottom of the borehole.

10 2. The rotary cone rock bit as set forth in claim 1 wherein an angle
formed between the diamond cutting surface and a wall formed by the formation
is between five and twenty five degrees with a leading edge formed by the
cutting face being further away from the wall than a trailing edge formed by the
15 diamond cutting surface.

 3. The rotary cone rock bit as set forth in either one of claims 1 or 2
wherein the extended insert is a right angle cylindrical body, the cutting surface
is perpendicular to an axis of the body, and the diamond cutting surface is
20 formed from polycrystalline diamond.

 4. The rotary cone rock bit as set forth in either one of claims 1 or 2
wherein the diamond cutting surface is oblique to an axis of the cutter body.

25 5. The rotary cone rock bit as set forth in either one of claims 1 or 2
wherein the edge formed by the cylinder at the exposed diamond surface is
chamfered or radiused.

 6. A rotary cone rock bit for drilling boreholes in an earthen formation
30 comprises one or more rotary cones rotatably retained on a bearing connected
to a body of the rock bit, each cone comprises a circumferential heel row with
polycrystalline diamond inserts spaced within the heel row, each of the diamond
inserts comprising an exposed diamond surface that is about adjacent to the
formation, and characterized by

35 the diamond insert being a right angle cylindrical body with an edge
formed by the cylinder at the exposed diamond surface is chamfered or radiused
to reduce cracking and chipping of the diamond, the inserts serving to maintain

1 a constant diameter borehole wall formed by the formation as the rotary cone
rotates against a bottom of the borehole.

5 7. The rotary cone rock bit as set forth in any one of the preceding
claims wherein the extended insert is a right angle cylindrical body, the diamond
cutting surface is about half diamond, the remaining half of the cutting surface
is an ultra hard material forming the insert body, and the diamond portion of the
insert is oriented toward a direction of rotation of the rotary cone.

10 8. The rotary cone rock bit as set forth in any one of claims 1, 2 or 4
wherein the diamond cutting surface of the insert is comprised of individual
diamond segments imbedded in the surface.

15 9. A rotary cone rock bit for drilling boreholes in an earthen formation
comprising one or more rotary cones rotatably retained on a bearing connected
to a body of the rock bit, each cone comprising a circumferential heel row, and
characterized by two or more rows of heel inserts on different radial distances
from a cone axis, at least one row containing diamond faced inserts, the diamond
faced inserts being on a shorter radial distance than another heel row containing
inserts formed from tougher ultra hard material.

20 10. The rotary cone rock bit as set forth in claim 9 wherein the tougher
ultra hard material comprises cemented tungsten carbide.

25 11. A rotary cone rock bit substantially as
described herein with reference to the accompanying
drawings.

30

35

Patents Act 1977 Examiner's report to the Comptroller under Section 17 the Search report)	Application number GB 9411505.2
Relevant Technical Fields (i) UK Cl (Ed.M) E1F (FFD, FGA, FGB, FGC) (ii) Int Cl (Ed.5) E21B 10/52	Search Examiner D J HARRISON
Databases (see below) (i) UK Patent Office collections of GB, EP, WO and US patent specifications. (ii) ONLINE DATABASES: WPI	Date of completion of Search 6 SEPTEMBER 1994 Documents considered relevant following a search in respect of Claims :- 1 to 5, 11

Categories of documents

X: Document indicating lack of novelty or of inventive step.	P: Document published on or after the declared priority date but before the filing date of the present application.
Y: Document indicating lack of inventive step if combined with one or more other documents of the same category.	E: Patent document published on or after, but with priority date earlier than, the filing date of the present application.
A: Document indicating technological background and/or state of the art.	&: Member of the same patent family; corresponding document.

Category	Identity of document and relevant passages		Relevant to claim(s)
X,E	GB 2274129 A	(SMITH INTERNATIONAL INCORPORATED) 13 July 1994. Whole document, but see particularly Figures 9-12	1,4,5
A	EP 0476352 A	(HUGHES TOOL COMPANY) see inserts 41	1
A	US 5119714 A	(SCOTT et al) see inserts 83	1
A	US 4940099 A	(DEANE et al) see inserts 36	1

Databases: The UK Patent Office database comprises classified collections of GB, EP, WO and US patent specifications as outlined periodically in the Official Journal (Patents). The on-line databases considered for search are also listed periodically in the Official Journal (Patents).